substituted and their associated equations were originally included and are fully supported by provisional application 60/308,587, to which the present application claims priority. Further still, the present application is one of five co-pending applications that were filed simultaneously and with essentially common disclosures. Three of the five co-pending cases were filed free of any typographical errors. For instance, all substituted symbols (in particular, symbols in connection with the description of FIG. 1d) are supported by co-pending application 10/050,529, having at least one common inventor with the present application. Applicants respectfully submit that this amendment adds no new matter, is fully supported by the instant and priority disclosures, and merely corrects typographical errors and, therefore, should be entered.

If the Examiner believes that a telephone conference or interview would advance prosecution of this application in any manner, the undersigned stands ready to conduct such a conference at the convenience of the Examiner.

It is believed that no fees are due in connection with the filing of this Preliminary Amendment. In the event it is determined that a fee is necessary to maintain the pendency of this application, the Commissioner is hereby authorized to charge or credit the undersigned's Deposit Account No. 50-0206.

Respectfully submitted,
HUNTON & WILLIAMS

Date: April 18, 2002

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ATTACHMENT A - REVISIONS TO SPECIFICATION

At page 13, line 21, delete "!" and insert --±--;

line 22, delete "!" and insert --±;

line 24, delete "!" and insert --±--.

At page 14, line 5, delete "♌ + ♋" and insert --$\gamma + \delta$--;

line 9, delete "♌" and insert --γ--;

line 11, delete "♋" and insert --δ--;

At page 17, line 4, delete "♋ < ♌" and insert --$\alpha < \beta$--;

line 7, delete "♋" and insert -- α--;

line 7, delete "♌" and insert --β--.

At page 19, line 16, delete "∃"(both occurrences) and insert --·--;

line 17, delete "∃"(both occurrences) and insert --·--;

line 18, delete "↑" and replace with --···--;

At page 21, line 13, delete "∃"(both occurrences) and insert --·--;

line 14, delete "∃"(both occurrences) and insert --·--;

line 16, delete "↑" and replace with --···--;

At page 23, line 5, delete "♌" and insert --γ--;

line 6, delete "♋" and insert --δ--;

At page 25, line 6, delete "♋ < ♌" and insert --$\alpha < \beta$--;

line 9, delete "♌" and insert --γ--;

line 10, delete "♋" and insert --δ--.

At page 30, line 21, delete "{" and insert --≅--.

At page 46, line 2, delete "③" and insert --μ--.

APPENDIX B - SPECIFICATION AFTER AMENDMENTS

Page 13, second paragraph, lines 19-29, replace this paragraph in its entirety with the following:

FIG. 1d is an example of a timing diagram of an activation sequence. As illustrated, STUR may initiate Cr, lasting a duration of t_{cr}, which has a nominal value of 1 second with ± 20 millisecond tolerance. Time from the end of Cr to a beginning of Sc is represented by t_{crsc}, which has a nominal value of 500 millisecond with ± 20 millisecond tolerance. After a time t_{crsc}, STUC may initiate Sc. Time from the end of Cr to a beginning of Sr is represented by t_{crsr}, which has a nominal value of 1.5 second with ± 20 millisecond tolerance. After a time t_{crsr}, STUR may initiate Sr. After Sc, STUC may initiate Tc. After Sr, STUR may initiate Tr. After Tc, STUC may initiate Fc. At approximately the same time, $Data_c$ and $Data_r$ may be initiated by STUC and STUR, respectively. Time from the beginning of Cr to the beginning of $Data_r$ is represented by $t_{Actdata}$, which has a nominal value of 15 seconds.

Page 14, first paragraph, lines 1-11, replace this paragraph in its entirety with the following:

If the SNR is calculated in the time domain, one method to determine PBO is according to the equations shown below.

$$SNR_{dB} = 10\log_{10}\left(\frac{P_{signal+noise}}{P_{noise}}\right) = 10\log_{10}\left(\frac{\sum_{n=0}^{M-1}|[s(n)+w(n)]|^2}{\sum_{n=0}^{M-1}|w(n)|^2}\right) \qquad (1)$$

$$PBO_{dB} = SNR_{dB} - (\gamma + \delta + SNR_{min}) \qquad (2)$$

$s(n) = n^{th}$ sample of the received signal
$w(n) = n^{th}$ sample of the received noise
M = window length in samples used to compute average
$P_{signal+noise}$ = power of signal + noise
P_{noise} = power of noise only

where γ represents a required margin in dB ($\geq$ 0 dB, example: G.SHDSL Annex B margin is 6 dB); SNR_{min} represents a minimum SNR in dB needed to obtain the specified BER, and δ represents an implementation loss in dB.

Page 16, second paragraph, lines 12-22 and page 17, lines 1-9, replace this paragraph in its entirety with the following:

Using the geometric mean, a SNR of the channel may be computed using the following:

$$SNR \cong \left[\left[\prod_{k=\alpha}^{\beta} \frac{|Y(k) - \hat{W}(k)|^2}{|W(k)|^2} \right]^{\frac{1}{\beta-\alpha+1}} \right] \tag{6}$$

$$SNR \cong 10\log_{10} \left[\left[\prod_{k=\alpha}^{\beta} \frac{|Y(k) - \hat{W}(k)|^2}{|W(k)|^2} \right]^{\frac{1}{\beta-\alpha+1}} \right] = \frac{10}{\beta-\alpha+1} \sum_{k=\alpha}^{\beta} \log_{10} \left[\frac{|\hat{S}(k)|^2}{|W(k)|^2} \right] \tag{7}$$

which may be rewritten in the following manner to filter cells with negative or zero SNR

$$D'_k = \log_{10} \left[\frac{|\hat{S}(k)|^2}{|W(k)|^2} \right] \tag{8}$$

$$D_k = \begin{cases} D'_k & D'_k > 0 \\ 0 & otherwise \end{cases} \tag{9}$$

$$SNR_{dB} = \frac{10}{\beta-\alpha+1} \left(\sum_{k=\alpha}^{\beta} D_k \right) \tag{10}$$

where $0 < \alpha < \beta <$ N-1; $\hat{S}(k)$ represents an estimate of k^th^ frequency sub-band of a received signal spectrum; $\hat{W}(k)$ represents an estimate of k^{th} frequency sub-band of a received noise spectrum; $Y(k)$ represents a k^{th} frequency sub-band of signal plus noise spectrum; α represents a

starting sub-band; β represents an ending sub-band; D_k represents one or more sub-bands with SNR greater than zero; D'_k represents SNR for k^{th} sub-band.

Page 19, lines 7-21, replace this paragraph in its entirety with the following:

Equation (15) is described in "The Fast Fourier Transforms and it's Applications" by E. Oran Brigham –1988 – equation 6.16, page 97.

The first cosine and sine terms may be found using the equations below.

$$R_0 = \cos\left(\frac{4\pi}{N_{real}}\right) \tag{16}$$

$$I_0 = -\sin\left(\frac{4\pi}{N_{real}}\right) \tag{17}$$

where

N_{real} = real FFT size

R_0 = zeroth sample of real part of exponential weight

I_0 = zeroth sample of imaginary part of exponential weight

The equations to recursively compute the transform weights are given below:

$$R_m = R_0 \cdot R_{m-1} - I_0 \cdot I_{m-1} \tag{18}$$

$$I_m = I_0 \cdot R_{m-1} + R_0 \cdot I_{m-1} \tag{19}$$

where m = 1, 2, $\cdots \frac{N_{real}}{4}$

$R_m = m^{th}$ sample of real part of exponential weight

$I_m = m^{th}$ sample of imaginary part of exponential weight

Page 21, lines 10-16, replace this paragraph in its entirety with the following:

Equations (18) and (19) may be modified slightly and then used with the above initializers to compute the new weights.

$R_m = R_0 \cdot R_{m-1} - I_0 \cdot I_{m-1}$ (28)

$I_m = I_0 \cdot R_{m-1} + R_0 \cdot I_{m-1}$ (29)

where $m = 1, 2, \cdots \frac{N_{real}}{2}$

Page 22, fifth paragraph, lines 26-28 and page 23, lines 1-6, replace this paragraph in its entirety with the following:

If the SNR is calculated in the time domain, a method to compute the capacity may include measuring the silence power (noise), P_{noise}, and then the received power (signal + noise), $P_{signal+noise}$, and finding the capacity, C, using the equation below.

$$C = B\log_2\left(1 + \frac{P_{signal}}{P_{noise}10^{\frac{(\Gamma - G + \gamma + \delta)}{10}}}\right) = B\log_2\left(1 + \frac{SNR}{10^{\frac{(\Gamma - G + \gamma + \delta)}{10}}}\right)\frac{bits}{second} \qquad (30)$$

where Γ represents a gap from a theoretical channel capacity for PAM signals, in dB; G represents a coding gain of a Trellis decoder in dB; B represents a transition bandwidth; γ represents a required margin in dB (e.g., G.SHDSL Annex B margin is approximately 6 dB); and δ represents an implementation loss in dB.

Page 24, third paragraph, lines 27-28 and page 25, lines 1-11, replace this paragraph in its entirety with the following:

Starting with equation (30) above, an overall capacity may be determined by summing capacities for each individual sub-band as shown by equation (33) below.

$$C \cong B_s \sum_{k=\alpha}^{\beta} \log_2\left(1 + \frac{|Y(k) - \hat{W}(k)|^2}{|\hat{W}(k)|^2\, 10^{\frac{(\Gamma - G + \gamma + \delta)}{10}}}\right)$$

$$= B_s \sum_{k=\alpha}^{\beta} \log_2 \left(\frac{|\hat{W}(k)|^2 10^{\frac{(\Gamma - G + \gamma + \delta)}{10}} + |Y(k) - \hat{W}(k)|^2}{|\hat{W}(k)|^2 10^{\frac{(\Gamma - G + \gamma + \delta)}{10}}} \right)$$

$$= B_s \left(\sum_{k=\alpha}^{\beta} \log_2 \left(|\hat{W}(k)|^2 10^{\frac{(\Gamma - G + \gamma + \delta)}{10}} + |\hat{S}(k)|^2 \right) - \sum_{k=\alpha}^{\beta} \log_2 \left(|\hat{W}(k)|^2 10^{\frac{(\Gamma - G + \gamma + \delta)}{10}} \right) \right) \quad (33)$$

where $B_s = \frac{B}{(\beta - \alpha + 1)}$; $0 < \alpha < \beta <$ N-1; B_s represents a sub-band width in Hz; $\hat{S}(k)$ represents an estimated "signal only" power; Γ represents a gap from a theoretical channel capacity for PAM signals, in dB; G represents a coding gain of a Trellis decoder in dB; γ represents a required margin in dB (e.g., G.SHDSL Annex B margin is approximately 6dB); δ represents an implementation loss in dB, α represents an index of a first sub-band and β represents an index of a last sub-band.

Page 30, fifth paragraph, lines 17-23 and page 31, lines 1-5, replace this paragraph in its entirety with the following:

As shown in FIG. 7, an output of the precoder 710 may have an approximately flat power spectrum. Keeping this in mind while tracing the signal paths in the above block diagram, the following may apply:

$$X(f) \cong K = \text{constant} \quad (37)$$

$$Y(f) = X(f)H_{txf}(f)H_{ec}(f) + T_f(f)H_c(f) + W(f) \quad (38)$$

$$Z(f) = X(f)H_{dec}(f) \quad (39)$$

$$\begin{aligned} E(f) &= Y(f) - Z(f) = [H_{txf}(f)H_{ec}(f) - H_{dec}(f)]X(f) + T_f(f)H_c(f) + W(f) \\ &= [H_{txf}(f)H_{ec}(f) - H_{dec}(f)]K + T_f(f)H_c(f) + W(f) \quad (40) \end{aligned}$$

where $R_e(f)$ is defined as $[H_{txf}(f)H_{ec}(f) - H_{dec}(f)]K$ wherein $R_e(f)$ represents residual echo spectrum, then $E(f) = R_e(f) + T_f(f)H_c(f) + W(f)$.

Page 45, fifth paragraph, lines 28-29 and page 46, lines 1-8, replace this paragraph in its entirety with the following:

The optimum shift points may be determined by software. The following table lists the gear-shift point in samples and the right shift (e.g., power of two) division of the weights. These gears may be used in the initial training. While in steady state, a single gear may be used and may be approximately ½ the smallest μ in the table.

Gear#	0	1	2	3	4	5
Samples	2000	598	1427	3188	7241	15000
Right Shift	3	4	5	6	7	8